Oxide Ceramic Matrix Composites – Manufacturing, Machining, Properties and Industrial Applications

Oxide ceramic matrix composites (O-CMC) combine high temperature stability, low density, high strength and good corrosion resistance with a damage-tolerant quasi-ductile fracture behaviour enabling a variety of applications with demanding thermal and mechanical requirements.

Introduction
Ceramics generally show excellent temperature stability, low density, high hardness, good corrosion and wear resistance making them interesting materials for applications with demanding thermal and mechanical requirements. However, the use of monolithic ceramics as structural materials is often limited due to their brittle fracture behaviour. By reinforcing ceramics with ceramic fibres and tailoring the fiber-matrix interface, damage-tolerant quasi-ductile fracture behaviour can be achieved. These CMC materials can substitute metallic components in high temperature environments bringing advantages in terms of weight reduction, increase in thermal efficiency by increasing process temperatures or prolonged service life time and reduced maintenance costs [1, 2]. CMCs exist as non-oxide (NO-CMC) and all-oxide types (O-CMC). Comparing both types of CMC materials, O-CMCs exhibit lower maximum application temperatures, but are easier to fabricate, less expensive, and resistant to oxidation.

O-CMC materials are developed since some decades, have been continuously improved, and are currently commercialised by a few companies like COI-ATK/US, WPX Faserkeramik GmbH/DE and Walter E. C. Pritzkow Spezialkeramik (WPS)/DE. Improvement of O-CMC materials is constantly evolving with main efforts made in universities and research centers in the USA, France and Germany. Being a new class of material, O-CMC slowly entered into first applications like furnace components and flame tubes. These first applications demonstrated the potential of O-CMC materials and gave opportunities to develop the materials, their processing and the design layout of O-CMC components further. Currently, O-CMC components enter more and more applications and number items increase making series production processes necessary.

In this article some of the achievements are presented that have been made between WPS and Fraunhofer Institute for Silicate Research (ISC)/Center for High Temperature Materials (HTL)/DE who are collaborating in O-CMC development for more than 10 years.

Oxide ceramic matrix composites
O-CMCs are composite materials consisting of an oxide ceramic matrix reinforced by oxide ceramic reinforcing fibres. As reinforcing fibres, oxide fibres like Nextel TM 610 or 720 from 3M/US are typically used, often in form of textile fabrics.

Fig. 1
Oxide ceramic fibres as woven fabric

Keywords
oxide ceramic matrix composites (O-CMC), fabrication techniques, material properties, industrial applications
As matrix components, different ceramic compositions like Al₂O₃ or mixtures like Al₂O₃–SiO₂, Al₂O₃–ZrO₂ are used. The materials exhibit low density, e.g. 1/3 of the density of high-temperature steels and super alloys, high bending strength, high thermal shock resistance and good stability in oxidising and moisture-rich atmospheres [3–6]. Applications of O-CMC materials are limited to about 1200 °C, because then degradation of the mechanical performance of the reinforcing fibres is observed [7]. The reason for the degradation of the mechanical properties is a coarsening of the ceramic grains of the fibres, which lead to reduced tensile strength values [8]. Thus, the maximum application temperature of O-CMC materials is limited to about 1150 °C for long-term use and up to 1200 °C for short term exposure. To achieve damage-tolerant fracture behaviour of O-CMC materials, a weak interface between the fibres and the matrix is required [9]. When the material is under load and starts to crack, the cracks are deflected at the weak fiber-matrix interface. These deflection mechanisms dissipate energy and catastrophic failure is shifted to much larger strain values. Thus, O-CMCs can show strain-to-failure values of up to 0.6 %, whereas monolithic ceramics exhibit strain-to-failure values below 0.1 % (Fig. 2).

The weak fibre-matrix interface is basically realized by two concepts. First, the ceramic fibres are coated with a ceramic layer, which provides the weak interface between the fibre and the matrix material (“weak interphase concept”) [10]. This concept is realized when rather dense O-CMC materials are needed [3, 11]. More typically, the matrix of the O-CMC material is porous and less stiff than the reinforcing fibres (“weak matrix concept”) [12]. In this case, the weak fibre-matrix interface is given due to the fact that the matrix is only partially bonded to the fibre [13]. Thus, no fibre coating is needed.

A disadvantage of using a porous matrix is its low intrinsic strength which brings limitations to the matrix-dominated properties of the composite. If a higher strength of the matrix is desired, the porosity needs to be lowered. This can be realized by sintering the O-CMC material at higher temperatures. One problem caused by the higher sinter temperatures is crack formation in the matrix. At high sintering temperatures the matrix shows significant volume shrinkage, whereas the reinforcing fibres or fabrics form a rigid network. Thus, matrix cracks occur with this approach, which limits the mechanical performance of the composite materials. The approach of WPS and Fraunhofer ISC/HTL is to maximize the strength of the ceramic matrix and while minimizing its volume shrinkage during sintering. This is achieved by realizing a multiscale design of the matrix microstructure using different grain size fractions. In this case a solidification of the matrix without cracking is possible, which leads to O-CMC materials with good mechanical performance.

**Manufacturing processes of textile-based oxide ceramic matrix composites**

WPS and Fraunhofer ISC/HTL use three different techniques to fabricate components made of textile-based O-CMC materials. The manufacturing methods are well-established for fibre-reinforced plastics and have been adapted to the requirements for producing O-CMC components.

**Lamination process (method 1)**

In this process, fabrics of oxide ceramic fibres are first infiltrated with a slurry of matrix material. Then, the infiltrated fabrics are draped on a tool. Different layers of draped fabrics are pressed using a scraper or a roller (Fig. 3). This method leads to the lowest fibre volume contents resulting in the lowest strength values of the materials. Nevertheless, the process is very simple and fast, and is used for components with lower requirements on mechanical performance.

**Mould pressing (method 2)**

Infiltrated fabrics are laminated upon each other, put into a press mould and compacted by applying pressure (Fig. 4). Compacting can be performed under defined pressure or to a defined thickness of the infiltrated fabrics by using mechanical stoppers. After pressing, the part is dried in a drying oven under moderate temperatures. Alternatively, the part can also be warm-pressed so that the drying process is not necessary. Using this method, higher and well-defined fibre volume contents can be realised in comparison to method 1. The method is used for high-quality components, allows near-net shape manufacturing, but is limited to parts with rather low complexity.
Machining of fibre-reinforced oxide ceramic matrix composites

The classical method to machine fibre-reinforced oxide ceramic matrix composites is by using diamond tools like diamond wire saws, diamond cut-off wheels, diamond drill bits or mounted points. The methods are used to carve out arbitrary shapes or hole patterns from complex 3-dimensional components or to realise threads (Fig. 7a, b). Another option is to carve out complex shapes with smooth surfaces from thick O-CMC plates. In this case a lot of waste is produced which should be avoided if possible.

The material can also be machined by using milling cutters based on high-speed steel (HSS cutters) or polycrystalline diamond (PCD cutters) (Fig. 8). The method can be used to machine complex shapes, is faster than diamond based grinding can be stored for several weeks at room temperature (Fig. 6).

Vacuum-assisted lamination process (method 3)

Like in method 1, infiltrated layers of fabrics are draped on a tool. Then, peel foils are put around the fabrics. The part is put into a bag which is evacuated (Fig. 5). Using this method, high fibre volume contents, high densities of the matrix and complex shapes can be realized. The technique is used to fabricate components with high complexity and very high strength values.

Fabrication of prepregs for O-CMC lamination

The lamination process (method 1 to 3) is suitable for individual items and small series production. With an increasing number of items components and increasingly demanding specifications for components, for example O-CMC parts for gas turbines, automated, reproducible and standardized production methods become a necessity. For these reasons, WPS and Fraunhofer ISC/HTL are currently developing a prepreg production process for O-CMC parts. The process allows a defined infiltration of fabrics in terms of mass and volume using an aqueous suspension of ceramic powders and organic binders. During the infiltration process the fabric is directly put between two carrier foils. The produced prepregs can be stored for several weeks at room temperature (Fig. 6).
methods, but the surfaces are also slightly rougher.

Another method to machine O-CMC components is laser machining. It is used to realise complex hole patterns in plates and tubes in a fast and cost-effective manner (Fig. 9). The method provides high precision. In contrast to diamond grinding, laser machining can be used for large number of items.

Waterjet cutting is an alternative to laser machining (Fig. 10). Typically, an abrasive medium is added to the water to be able to cut the ceramic materials. Due to the abrasive media, the cutting line is less smooth when compared to laser cutting. Another disadvantage is the possible occurrence of material delamination due to the waterjet.

Properties of O-CMC materials

Recently, two standard high-end O-CMC materials, named Keramikblech® FW12/30 and Keramikblech® SA12 have been developed by WPS and Fraunhofer ISC/HTL (Tab. 1). Fig. 11 shows a comparison of the performance of different types of commercially available O-CMC materials.

Industrial applications of O-CMC components

O-CMC components can substitute metallic parts in high temperature processes. The advantages of using O-CMCs are

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weight reduction due to reduced density and mass, increase in thermal efficiency by increasing process temperatures or prolonged service lifetime and reduced maintenance costs. The initial higher purchase costs of O-CMC components often amortize during operation bringing overall cost savings. Moreover, O-CMC components can enable high temperature processes being not possible with metallic parts (see lift gates in following sections).

**Flame tubes based on O-CMC**

O-CMC materials can be used for flame tubes in industrial applications as a substitute for metallic flame tubes leading to a tremendous increase in service lifetime (Fig. 12). For example, in a baking line for producing crispbread, metallic flame tubes were used that had a service lifetime of about 1000 h. The replacement of these components necessitated 6 shut-downs of the production plant per year leading to long production downtimes and huge costs. Searching for an alternative, the metallic flame tubes were exactly rebuilt by a 1:1 copy using O-CMC materials. The O-CMC flame tubes could be directly integrated into the production plant. The service lifetime of the O-CMC flame tubes is larger than 60 000 h. This results in enormous cost savings due to less production downtimes and lower maintenance efforts. Due to these cost savings, the higher purchase costs of the O-CMC flame tubes in comparison to the metal based counterparts charged off quickly. Also in other industrial applications O-CMC flame tubes have demonstrated largely increased service lifetimes in comparison to metallic flame tubes (Fig. 12).

**Lift gate for sinter metal production plant**

The potential of O-CMCs is also demonstrated in form of a lift gate in a sinter metal production plant (Fig. 13). The lift gate separates the debinding zone and the sintering zone. In the debinding zone temperatures of 600 °C and oxidizing conditions are used, whereas in the sintering zone temperatures between 1100 °C and 1280 °C and a N₂/H₂ atmosphere are used. Because of these harsh conditions, the gate could not be realised with metallic materials. Carbon/carbon composites were tested, but showed insufficient service lifetimes. A solution could be provided by building the lift gate from SiO₂-free O-CMC materials. With the O-CMC lift gate more than 1 000 000 open/close cycles have been demonstrated without interruption. For cycles times of 2 min, this means that the lift gate was used more than 40 months without interruption under these harsh conditions.

**O-CMC hot gas distributors**

In high temperature test rigs for testing sealings and exhaust systems for automotive applications, thin-walled and thermoshock resistant structures are needed for distributing the hot gas. Together with a thermally insulating intermediate layer, these structures are integrated in metallic frames. Hot gas with temperatures of 1200 °C produced by a fan burner is injected on one side of the distributors and led through the structures to the test components. When built completely from metallic materials, the distributors needed to be repaired several times during a 100 h test cycle because of cracked welded joints or extreme deformation of the metallic components. Using O-CMC materials for the distributors, several long time test runs were possible without any need for replacement or repair (Fig. 14).

**Modular design of O-CMC components**

There are many applications were a modular concept for a component or a component assembly is meaningful to minimize effects of thermal stresses. Beside the re-

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**Fig. 13**

O-CMC lift gate in sinter metal production plant operating at 1250 °C

**Fig. 14 a–c**

Hot gas distributors fabricated from O-CMC
The prototype is based on the O-CMC material Keramikblech® FW12. The part was manufactured near net-shape by combining several production techniques like lamination and mould pressing. Only the cavities were drilled and the steps within the holes were grinded. In beginning of 2015 MTU Aero Engines made a successful application test of these liner segments within an aero-engine. In the second half of 2015 the first hot gas ground-based test of the liner segment in an aero-engine will be started.

Summary

O-CMC materials combine the excellent mechanical and thermal properties of ceramics with a damage-tolerant quasi-ductile fracture behaviour making them attractive materials for the application in high temperature processes. Possible benefits of substituting metallic parts by O-CMC components are weight reduction, increased thermal/energy efficiency and prolonged service lifetime. O-CMC components like flame tubes, lift gates or charging racks have demonstrated their potential in various industrial high temperature applications. O-CMC parts for gas turbines are currently developed and tested.

References


